

AMD Treatment Site

Operation and Maintenance Report

Site: Gavazzi, LT 20
Watershed: Little Toby Creek

Date: 4/29/03
By: G.Swope / K.Hendrickson

Good Adequate Needs Action

Condition of Treatment System Components:

Vegetation:	X
Treatment Cells:	X
Wetland:	X
Rock Lined Waterways:	X
Water Control Structures:	X
Access Road:	X
Diversion	X
Mine Collection System	X

Activities: There has been a continuing problem with the inlet pipe to the WCS on the wetland plugging almost completely shut and raising the elevation of the water in the wetland until it overflows the dike. The increase in iron from 20 to 50 ppm after the collection system was put in the mine opening has caused considerable iron to precipitate in the wetland. There did not appear to be many cattails in the wetland but it is still early in the growing season. About 1/5 - ¼ of the surface of the first treatment bed has sandy, grainy, dark red iron precipitate between the rocks. This material is dense enough that when the cell is flushed, a small amount of water lays on the surface of the bed. Dug out the inlet end of the 6" wetland outlet pipe and cleaned the WCS.

Upper cell was flushed for about 3 hours until empty. Color of water was same as other flushes, a light creamy red. Water color did not change by end of flush.

There is a wet area about 25 feet down slope of the mine collection system. It is not wet enough to result in runoff and there is no iron staining. There was a small spring of good water about 25 feet to north of mine opening, it may be bleeding through the refuse. There was never any evidence that it did that before. There is no sign of an upwelling directly over the collection point. It is not anything that needs addressed at this time. The flow in the gully that carried the original mine flow seemed to be a little more than what it was last year. It is about 4-5 gpm at the top and increases as it comes down past the site to maybe 10+ gpm.

Action Needed: Need to install 90 degree elbow and short (1') standpipe on inlet end of settling basin outlet pipe or a floating dewatering device. Need to look at long term solution to the iron accumulation in the wetland outlet structure. Will flush again within 1-2 weeks to see if color of flush water will clear up.

Gavazzi AMD Site Site Visit / Operation and Maintenance Record

STATE <i>PA</i>	PROJECT <i>LTC</i>			
BY <i>OJ</i>	DATE <i>6-19-96</i>	CHECKED BY <i></i>	DATE <i></i>	JOB NO. <i></i>
SUBJECT <i>LT-20 Gavazzini</i>				SHEET 1 OF

Summary Sheet

Total Cost **\$104,455**
MAX Flow $Q = 70 \text{ gal/min}$

Flow 30 gpm
Acid 175 mg/l
Fe 21 mg/l
Al 6 mg/l
DO 1.2 mg/l
pH 3.1

mg 10 ppm < Fe 0.5 ppm < pH > 5.5 AL < 2 ppm
 $\begin{cases} \text{use } 500 \text{ ft }^2/\text{min} \end{cases}$

2.5 Days Retention time

Synthetic Process

2.0a
.28a
.08a
.04a
1.60a
 \rightarrow Pond & wet 4.0a

Disturbed Area

Saps
Darin
Wetland

Seeding

System - Saps - Setting Basin - wetland

STATE <u>PA</u>	PROJECT <u>LTC</u>			
BY <u>Gd</u>	DATE <u>6-19-96</u>	CHECKED BY _____	DATE _____	JOB NO. _____
SUBJECT <u>LT-2D GAVAZZI</u>	SHEET <u>2</u> OF _____			

~~Acid loading~~ - $30 \text{ gpm} \times 175 \text{ mg/l} \times 3.45 = 28613 \text{ g/d}$
 $28613 \text{ g/d} \div 454 \text{ g/l} = \underline{\underline{62.1 \text{ d}}}$

Size by Area -

$$28613 \text{ g/d} \div \frac{30 \text{ g/m}^2/\text{d}}{= 954 \text{ m}^2 \times 10.26 \text{ ft}^2/\text{m}^2 = 10263 \text{ ft}^2}$$

$$10263 \text{ ft}^2 \times 2 \text{ ft} / 27 \times 1.5 \text{ tons/ft}^3 = \frac{1140 \text{ tons}}{\text{yd}^3} = \underline{\underline{1711 \text{ tons}}}$$

Size for Detention $m = Q T / C$

$$m = 30 \text{ gpm} \times 1.5 \text{ ft}^3/\text{yd}^3 \times \frac{2 \text{ hrs} \times 60 \text{ min}}{.5} \times 4.951 \times 10^{-3} \text{ yd}^3/\text{min} = \underline{\underline{321 \text{ tons}}}$$

~~Add Dissolution~~ $m = Q T / C$

$$m = 30 \text{ gpm} \times 300 \text{ mg/l} \times \frac{3.785 \text{ l}}{1 \text{ gal}} \times 525600 \text{ m}^3 \times \frac{10}{145} \times \frac{10}{1000} \text{ mg} \times 2.205 \times 10^{-3} \text{ yd}^3/\text{mg} \times \frac{1 \text{ ton}}{2000 \text{ ft}^3}$$

$$m = \underline{\underline{548 \text{ tons}}}$$

$$\text{Total tons L.S.} = 321 + 548 = \underline{\underline{869 \text{ tons}}}$$

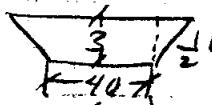
ft³ required for L.S.

$$869 \text{ tons} \times \frac{1 \text{ yd}^3}{1.5 \text{ tons}} \times 27 \text{ ft}^3/\text{yd}^3 = \underline{\underline{15642 \text{ ft}^3}}$$

Use 40' bottom width for Sides & 3.0 deg 9%

$$15642 \text{ ft}^3 \div 138 \text{ ft}^2/\text{ft.} = \underline{\underline{113 \text{ ft. (length)}}$$

$$A = 3 \times 40 + 2 \left(\frac{3 \times 6}{2} \right) = \underline{\underline{158 \text{ ft}^2}}$$



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SUBJECT <u>LTC-20</u>	SHEET <u>3</u> OF _____			
		Length	width	
	Top water	153	80	
	top Compost	129	56	
	top L.S.	125	52	
	Bottom	113	40	

Settling Basin - 24 hr Detention

$$\text{Size} = 309 \text{ rpm} \times 1 \text{ ft}^3 / 7.48 \text{ gal} \times 60 \text{ min} / \text{hr} \times 24 \text{ hr} / \text{d} = 5775 \text{ ft}^3$$

Add Fe accumulation

$$309 \text{ rpm} \times 21 \text{ mg/l} \times 5.45 = 3434 \text{ g/d} + 283168 \text{ cc/ft}^3 = .12 \text{ ft}^3$$

$$.12 \text{ ft}^3/\text{d} \times 365 \text{ d/yr} \times 25 \text{ yr} = \underline{1095 \text{ ft}^3}$$

$$\text{Total Storage} = 5775 + 1095 = 6870 \text{ ft}^3$$

- Use 6' storage depth if 20 ft bottom width

$$\text{Length} = 6870 \div 192 = \underline{36 \text{ ft}}$$

$$\frac{\pi r^2}{6 - \frac{r}{2}}$$

$$A = 6 \times 20 + 2 \left(\frac{6 \times 2}{2} \right)$$

$$A = 192 \text{ ft}^2 / \text{ft}$$

$$\text{Top width} = 20 + 2(16) = \underline{52 \text{ ft}}$$

$$\text{Top length} = 36 + 2(16) = \underline{68 \text{ ft}}$$

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BY <u>GS</u>	DATE <u>6-19-96</u>	CHECKED BY _____	DATE _____	JOB NO. _____
SUBJECT <u>LT-20</u>	SHEET <u>4</u> OF _____			

Aerobic wetland - ~~soil~~ removal in basin

$$\text{Fe lancing} = 3434 \text{ g/d} \times .20 = 687 \text{ g/d} \div 10 \text{ g/m}^2/\text{d} = \\ 68 \text{ m}^2 \times 10.76 \text{ ft}^2/\text{m}^2 = 739 \text{ ft}^2$$

Bottom dimensions - use 25' x 40'

$$\begin{array}{l} \text{Top width} - 25 + 2(6) = \underline{\underline{37 \text{ ft}}} \\ \text{Top Length} - 40 + 2(6) = \underline{\underline{52 \text{ ft}}} \end{array}$$

$\sqrt{\frac{1}{3} \times \frac{1}{2}}$

Water Conveyance

Discharge to Saps

Saps to Basin

Basin to wetland

wetland to drainage way

6" SDR

6" SDR

Rock w/w

Rock w/w

Quantities

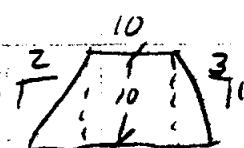
$$\text{Compost } 129 \times 56 \times 1.0 / 27 \times \frac{ton}{2} = 134 \text{ tons} \times \frac{40 \text{ ft}}{ton} = \underline{\underline{5360}}$$

$$\text{Limestone } 869 \text{ tons} \times \frac{40 \text{ ft}}{ton} = \underline{\underline{17380}}$$

Earth work

Saps 153 x 80

$$\begin{aligned} \text{Volume} &= 153 \times 350 + 80 \times \left(\frac{350 \times 0}{2} \right) + 80 \left(\frac{350 \times 0}{2} \right) \\ &= 81550 \text{ ft}^3 / 27 = \underline{\underline{3020 \text{ yd}^3}} \end{aligned}$$



$$\begin{aligned} A &= (10 \times 10 + \frac{10 \times 20}{2} + \frac{10 \times 30}{2}) \\ A &= 350 \text{ ft}^2 / 4 \end{aligned}$$

