Spaghetti Hole Passive Treatment System SRI O&M TAG Project #58 Request #1 OSM PTS ID: PA-64

<u>Requesting Organization:</u> Altoona Water Authority <u>Requesting Organization Representative:</u> Amy Sipes <u>Municipality/County:</u> Altoona, Blair County <u>Dates of work performed:</u> 5/10/2019 to 7/11/2019

<u>Initial Request</u>: On 9/10/2018, the Altoona Water Authority (AWA) requested assistance to evaluate and make recommendations about properly maintaining the Spaghetti Hole passive treatment. They indicated that a portion of the water was bypassing the system. The evaluation and recommendations were to be conducted in conjunction with Saint Francis University staff and students.

<u>Observations and Identified Needs</u>: Water quality passing through the Successive Alkalinity Producing System (SAP) (aka Vertical Flow Pond (VFP)) outlet was good. The inlet to the SAP was eroded but stable, likely due to ATV activity. All stop logs for the SAP outlet were in place. It appeared that the SAP outlet weir had been reconfigured and the staff gauge had not been adjusted to the new weir height. Access road repair including erosion control is an ongoing maintenance need at this site as the road is very long. Overflow from the SAP bypassing treatment was the primary water quality related concern.

<u>Work Completed:</u> SAP stop logs were removed from the Agri Drain box to determine if adjusting head pressure would allow an increased amount of flow to pass through the SAP. After two days, there was no longer an overflow at the treatment system bypass. To further assess the media, test pits were dug in four locations throughout the pond. Most of the organic media appeared to be in good condition. Much of the limestone was clean enough to have void space, with only a few places close to appearing impermeable due to iron and aluminum precipitates. The tests pits were filled and some of the stop logs were re-installed to allow water to fill the pond.

<u>Current Recommendations</u>: Confirm the elevation of the staff gauge at the SAP outlet is adjusted to the proper elevation relative to the new weir height for flow measurements. Continue to monitor the SAP water level to determine the proper amount of stop logs required to maintain water levels on top of the media but not bypassing the SAP overflow pipe. Based on available data, even when the current system is net alkaline, aluminum solids are usually present at the system effluent.

<u>Future Considerations:</u> When the stop logs in the Agri Drain box are configured to direct flow through the SAP treatment media, the overall water chemistry is typically alkaline with low iron and aluminum concentrations. The system effluent chemistry (Point SHSEDOUT) indicates that the system can neutralize all the acidity (e.g., the effluent typically has a circumneutral pH and negative acidity) but has difficulty settling sufficient aluminum solids to consistently result in concentrations below 1 mg/L. This system was constructed in 2002 and for a system of this age, typically alkaline effluent is a noteworthy success. However, the test pits did document that plugging of the limestone layer with aluminum (whitish) solids is occurring to a degree. In order to provide the most cost-effective enhancement of the existing system, a proposed conceptual design has been developed to rehabilitate the system using the existing components in their current configuration with improvements that will continue to neutralize acidity and precipitate aluminum while providing enhanced solids removal. The improvements discussed below are noted on the Conceptual Design prepared as part of this report.

The sedimentation pond is relatively small and is essentially filled with sediment and vegetation. To provide additional settling capacity, it is recommended that the pond be cleaned to restore at least the original water volume and if no liner is present and soil conditions indicate that leakage would not be anticipated, the bottom should be excavated to provide additional solids storage volume. In order to help increase settling effectiveness, two floating widowed baffle curtains should be installed. Material removed from the sedimentation pond will be placed in the proposed dewatering basin.

The existing SAP pond has a compost layer approximately one foot to two feet thick with overlying sediment. The purpose of a compost layer in a SAP of this vintage is to cause ferric iron (Fe^{+3}) to be reduced to the ferrous form (Fe⁺²) to keep iron from precipitating within the underlying limestone layer. Since 2016, the average total iron concentration in the raw (influent) water has been less than 1 mg/L which does not justify the presence of organic material. The test pits excavated in 2019 show a notable accumulation of aluminum solids in the limestone, which is not unexpected as the presence of organic material does not prevent the precipitation of aluminum solids. It is recommended that the compost be removed and placed as a soil amendment in the area around the treatment system and that the first 1-2 feet of limestone be washed to remove as much of the aluminum solids as feasible. The underdrain piping is PVC and, if exposed, would likely be broken and need significant repairs. Several temporary wash basins could be constructed within the SAP to facilitate cleaning of the limestone that appears to be AASHTO #3 size aggregate. Care should be taken during the washing process to capture the precipitate in the wash basins and transfer the material into the dewatering basin as possible and avoid concentrating the material in the lower portion of the limestone and around the underdrain pipes. The cleaned limestone would be placed back into the SAP and leveled. The limestone cleaning is expected to remove the majority of metal precipitates but some metal solids would remain. Geochemical modeling using PHREEQ-n-AMDTreat beta v6.0 indicate the presence of metal solids enhances metal removal through sorption. Any underdrain pipes that may be damaged during limestone cleaning should be repaired using flexible rubber couplers and pipe of similar size and type. Over time it is expected that the solids formed by the proposed automatic flushing limestone-only vertical flow pond upstream of the SAP pond will clog the limestone in the SAP and that the SAP will function primarily as a settling pond. The size of the existing SAP pond is conducive for this purpose it will provide over four times the settling capacity as the existing sedimentation pond. The existing SAP pond emergency spillway would then function as a primary spillway.

Raw mine drainage entering the stabilization pond has moderate acidity (69 mg/L average) and aluminum (8 mg/L) with iron and manganese typically less than 1 mg/L and 4 mg/L, respectively. As there is typically no appreciable change in chemistry from the influent (Point SHRAW/STB) to the outlet of the stabilization pond (Point SHSTB/STB), and there is not a flow control device or sufficient volume to stabilize flow rate, it is proposed to reconfigure the initial treatment component, Stabilization Pond, to function as an automatic-flushing vertical flow pond (AFVFP). This will require minimal excavation as the elevation and size of current stabilization pond is conducive for gravity flushing to the SAP pond. Installing an AFVFP upstream of the SAP pond will result in accumulation of aluminum solids on top of the SAP limestone, however, the limestone layer will help to filter solids and allow equipment access for future maintenance activities. With limited excavation and grading, the existing stabilization pond should be able to accommodate approximately 4,000 tons of limestone. This would enhance system performance and extend the projected system life over 20 years.

The proposed maintenance activities will result in excess material. As noted above, organic material may be spread around the treatment system as a soil amendment. Other material removed from the existing treatment components will be placed in a newly constructed dewatering basin that will have sufficient capacity to facilitate the proposed improvements as well as future maintenance work. Flow measurements taken downstream of the proposed AFVFP will not accurately represent the actual inflow rate, therefore a H-flume is proposed at the inlet of the treatment system. The access road is about one mile long and needs significant drainage improvements,

grading, and surfacing. There are other passive treatment systems located between the Spaghetti Hole system and the public road that will benefit from improving the existing access road. The existing system is over 20 years old (constructed in 2002), therefore, the proposed improvements are recommended to be implemented in the near future to avoid a degradation of effluent water quality.

Attachments: Conceptual Design Site Plan, Site Overview Photo, AMDTreat Cost Calculations.

Photo Log

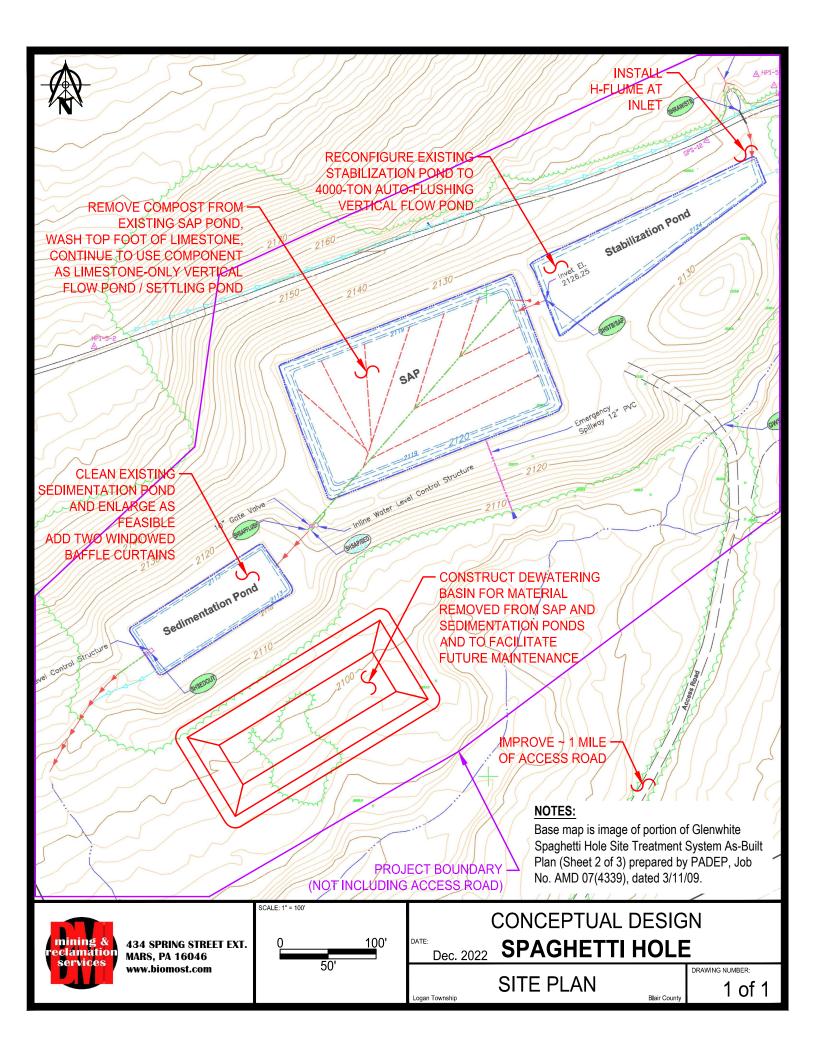


Top Left: Water level of the SAP dropped after lowering the stop logs.
Top Right: Stop logs removed from SAP outlet to lower the water level in the SAP pond.
Bottom Left: Much of the limestone was observed to still have void space, with only a few places appearing to be impermeable due to Fe and Al precipitates.
Bottom Right: The staff gauge was improperly set for the new weir elevation at the SAP outlet.

Passive Treatment Operation & Maintenance Technical Assistance Program Funded by PA DEP Growing Greener Stream Restoration Incorporated & BioMost, Inc. December 2022 O&M TAG 4 1117



Top Left: 10" PVC valve requires valve tool to open (standard 2" handle).
Top Right: Top of limestone layer with compost removed shows aluminum precipitates.
Bottom Left: Test pits revealed a 1" = 8" layer of precipitates overlaying 1.0' - 1.5' layer of compost with relatively clean limestone for a 20-year-old system.
Bottom Right: Close up of limestone layer with aluminum precipitates below compost layer.





Project O&M TAG

Site Name Spaghetti Hole



AMOTREAT

AMD TREAT AMD TREAT MAIN COST FORM

| Costs | AN | ID T | REAT MAIN |
|---------------------------|----------|----------|-----------|
| Passive Treatment | <u>A</u> | <u>s</u> | |
| Vertical Flow Pond | | | \$0 |
| Anoxic Limestone Drain | | | \$0 |
| Anaerobic Wetlands | | | \$0 |
| Aerobic Wetlands | | | \$0 |
| Manganese Removal Bed | | | \$0 |
| Oxic Limestone Channel | | | \$0 |
| Limestone Bed | 1 | 0 | \$264,400 |
| BIO Reactor | | | \$0 |
| Passive Subtotal: | | | \$264,400 |
| Active Treatment | | | |
| Caustic Soda | | | \$0 |
| Hydrated Lime | | | \$0 |
| Pebble Quick Lime | | | \$0 |
| Ammonia | | | \$0 |
| Oxidants | | | \$0 |
| Soda Ash | | | \$0 |
| Active Subtotal: | | | \$0 |
| Ancillary Cost | | | |
| Ponds | 1 | 0 | \$58,235 |
| Roads | 1 | 0 | \$39,583 |
| Land Access | | | \$0 |
| Ditching | | | \$0 |
| Engineering Cost | 1 | 0 | \$99,644 |
| Ancillary Subtotal: | | | \$197,462 |
| Other Cost (Capital Cost) | | | \$136,000 |
| Total Capital Cost: | | | \$597,862 |
| Annual Costs | | | |
| Sampling | | | \$0 |
| Labor | | | \$0 |
| Maintenance | | | \$0 |
| Pumping | | | \$0 |
| Chemical Cost | | | \$0 |
| Oxidant Chem Cost | | | \$0 |
| Sludge Removal | | | \$0 |
| Other Cost (Annual Cost) | | | \$0 |
| Land Access (Annual Cost) |) | | \$0 |
| Total Annual Cost: | | | \$0 |
| | 1 | 0 | |

| HMDIREH | |
|---------|---|
| | |
| 500.00 | gpm |
| 122.30 | gpm |
| 0.70 | mg/L |
| 0.20 | mg/L |
| 7.50 | mg/L |
| 3.30 | mg/L |
| 3.80 | su |
| 0.40 | mg/L |
| 1.20 | mg/L |
| | |
| | |
| 68.60 | mg/L |
| 495.40 | mg/L |
| 0.00 | mg/L |
| 10.00 | С |
| 0.00 | uS/cm |
| 0.00 | mg/L |
| 0.01 | mg/L |
| 18.3 | tons/yr |
| | |
| | 122.30 0.70 0.20 7.50 3.30 3.80 0.40 1.20 68.60 495.40 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 |

Total Annual Cost: per 1000 Gal of H2O Treated \$0.000 Company NameStream Restoration Inc.ProjectO&M TAGSite NameSpaghetti Hole

COMMENTS:

Raw water characteristics are based on monitoring 1/11/2016 through 10/12/2021 downloaded from www.datashed.org (accessed December 2022).

Chemistry is raw (Point SHRAW/STB) n=18

Flow measured at SAP (Point SHSAP/SED) n=14

Typical flow = Average

Design flow = Maximum

9.9 inch pipe used for AFVFP for 12 inch pipe.

Access road improvements representative, some areas will need more grading and/or aggregate than others.

Engineering Costs set at 20% (10% design, 6% permitting, 4% construction oversight)

Project O&M TAG

Site Name Spaghetti Hole

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Printed on 01/19/2023

Limestone Bed Name Convert Stabilization Pond to AFVFP



| U Opening Screen Water Parameter | | | | |
|-------------------------------------|--|--|--|--|
| | 1. Tons of Limestone Needed 2,943 | LSB Based on Acidity Neutralization | | |
| | 2. Tons of Limestone Needed 7,035 | C LSB Based on Retention Time 6. Ret | ention Time hours | |
| Influent Water Parameters | 3. Tons of Limestone Needed 11,386 | C LSB Based on Alkalinity Generation Rate 7. Alkalinity Gene | | |
| that Affect LSB | 4. Tons of Limestone Needed 4,000 | 2 | one Needed 4,000 tons | |
| Calculated Acidity | 5. Tons of Limestone Needed 1,297 | C LSB Based on Dimensions 9. Length at Top of Freeboard | ft 10. Width at Top ft of Freeboard ft | |
| 56.93 mg/L | | | | |
| Alkalinity | 11. % Void Space of LS. Bed 43.00 % | 29. Clearing and Grubbing? | LSB Sizing Summaries | |
| 0.40 mg/L | 12. System Life years | O 30a. Land Multiplier ratio | 48. Length at Top of Freeboard 266.78 ft | |
| | 13. Limestone Purity 85.00 % | O 30b. Clear/Grub Acres acres | 49. Width at Top of Freeboard 143.39 ft | |
| C Calculate Net | 14. Limestone Efficiency % | 31. Clear and Grub Unit Cost \$/acre | 50. Freeboard Volume 3,982 yd3 | |
| Acidity | 15. Density of Loose Limestone 94.30 lbs/ft3 | 32. Nbr. of Valves 0 nbr | 51. Water Surface Area 33,477 ft2 | |
| (Acid-Alkalinity) | | 33. Unit Cost of Valves 3500.00 \$ ea. | 52. Total Water Volume 2,366 yd3 | |
| Enter Net Acidity | | | 54. Limestone Surface Area 30,451 ft2 | |
| manually Net Acidity | 17. LS Placement Unit Cost 5.00 \$/yd3 | C AMDTreat Piping Costs | 55. Limestone Volume 3,142.06 yd3 | |
| (Hot Acidity) | Run of Slope Rise of Slope | 34. Total Length of Effluent / Influent Pipe | 56. Excavation Volume 5,508.9 yd3 | |
| 68.60 mg/L | 18. Slope of Pond Sides 2.0 : 1 | 35. Pipe Install Rate ft/hr | 57. Clear and Grub Area 0.0 acr | |
| | 19. Freeboard Depth 3.00 ft | 36. Labor Rate \$/hr | 58. Liner Area 5,535.0 ft2 | |
| Design Flow | 20. Free Standing Water Depth 2.0 ft | 37. Segment Len. of Trunk Pipe | 59. Theoretical Retention Time 9.09 hrs | |
| 500.00 gpm | 24. Limestone Depth 3.0 ft | 38. Trunk Pipe Cost \$/ft | LSB Cost Summaries | |
| Typical Flow | 25. Excavation Unit Cost 10.00 \$/yd3 | 39. Trunk Coupler Cost \$/coupler | 60. Siphon System Cost 18,000 \$ | |
| 122.30 gpm Total Iron | 23. Siphon System Cost 18000.0 \$ | 40. Spur Cost \$/ft | 61. Limestone Cost 160,000 \$ | |
| 0.70 mg/L | | 41. Spur Coupler Cost \$/spur | 62. Limestone Placement Cost 15,710 \$ | |
| Aluminum | Liner Cost | 42. "T" Connector Cost \$/T coupled | | |
| 7.50 mg/L | O No Liner | | | |
| Manganese | C Clay Liner | 43. Segment Len. of Spur Pipe ft/pipe seg. | | |
| 3.30 mg/L | 11. Clay Liner Unit Cost \$/yd3 | 44. Spur Pipe Spacing ft | \$ | |
| | 12. Thickness of Clay Liner ft | Custom Piping Costs | Ψ | |
| | C Synthetic Liner | Length Diameter Unit Cost | 67. Pipe Cost 15,600 \$ | |
| Record Number | 13. Synthetic Liner Unit Cost \$/yd2 | | 68. Total Cost 264,400 \$ | |
| 1 of 1 | | | | |
| | | 47. Pipe #3 ft in s | [▶] | |

AMD TREAT

Project O&M TAG

Site Name Spaghetti Hole

AMD TREAT

PONDS



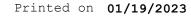
AMDTREAT

| Pond Name Dewatering Basin | | | | | | | |
|------------------------------------|---|--|-------------------|--|--|--|--|
| | Pond Design Based On: | 23. Revegetation Cost 3000.00 | \$/acre | | | | |
| | C Retention Time | 24. Cost of Baffles | \$ | | | | |
| | 1. Desired Retention Time hours | | _ | | | | |
| | | | | | | | |
| | 3. Sludge Removal Frequency times/year | Calculated Pond Dimensions per Po | nd | | | | |
| Opening Screen Water Parameters | 4. Titration? | 25. Length at Top of Freeboard 235 | ft | | | | |
| | 5. Sludge Rate gal sludge/ | 26. Width at Top of Freeboard 96 | ft | | | | |
| Influent Water Parameters | 6. Percent Solids | 27. Freeboard Volume 6,837 | yd3 | | | | |
| that Affect | | 28. Water Volume 5,262 | yd3 | | | | |
| Ponds | 7.Sludge Density Ibs./gal | 29. Estimated Annual Sludge | yd3/yr | | | | |
| Calculated Acidity | Pond Size | 30. Volume of Sludge | yd3/ removal | | | | |
| Alkalinity | 8. Pond Length at Top of Freeboard 235.000 ft | per Removal 31. Excavation Volume3.26 | acre ft | | | | |
| 0.40 mg/L | 9. Pond Width at Top of Freeboard 96.000 ft | 32. Excavation Volume 5,262 | yd3 | | | | |
| | Run Rise | 33. Clear and Grub Area 0.77 | acres | | | | |
| C Calculate Net | 10. Slope Ratio of Pond Sides 2.0 : 1 | 34. Liner Area 0 | yd2 | | | | |
| Acidity (Acid-Alkalinity) | 11. Freeboard Depth 2.0 ft | 35. Calculated Retention Time 35 | | | | | |
| Enter Net Acidity | 12. Water Depth 10.0 ft | Ponds Sub-Totals per Pond | | | | | |
| manually | 13. Excavation Unit Cost 10.00 \$/yd3 | 36. Excavation Cost 52,62 | 7 \$ | | | | |
| Net Acidity (Hot Acidity) | 14 Total Length of Effluent | 37. Pipe Cost 2,50 | 0 \$ | | | | |
| 68.60 mg/L | / Influent Pipe | 38. Liner Cost | 0 \$ | | | | |
| | 15. Unit Cost of Pipe 25.00 \$/ft Liner Cost | 39. Clearing and Grubbing Cost 2,33 | 0\$ | | | | |
| Design Flow | No Liner | 40. Revegetation Cost 77 | <mark>6</mark> \$ | | | | |
| 500.00 gpm Typical Flow | Clay Liner | 41. Baffle Cost | <mark>0</mark> \$ | | | | |
| 122.30 gpm | 16. Clay Liner Unit Cost \$/yd3 | | | | | | |
| Total Iron | 17. Thickness of Clay Liner ft | 42. Estimated Cost 58,23 | 5 \$ | | | | |
| 0.70 mg/L | O Synthetic Liner | | | | | | |
| Aluminum | 18. Synthetic Liner Unit Cost \$/yd2 | | | | | | |
| 7.50 mg/L Manganese | ☑ 19. Clearing and Grubbing? | _ | | | | | |
| 3.30 mg/L | © 20. Land Multiplier 1.50 ratio | | | | | | |
| Record Number | C 21. Clear/Grub Acres acres | | | | | | |
| 1 of 1 | 22. Clear and Grub Unit Cost 3000.00 \$/acre | Ð | | | | | |

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Project O&M TAG

Site Name Spaghetti Hole



AMD TREAT

ROADS

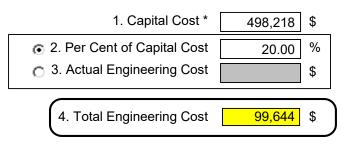


Road Name Access Road Improvements 1. Road Length 5300 | ft 14. Reveg Unit Cost \$/acre 3000.00 2. Road Width ft 15. Culvert Unit Cost \$/ft 12 50.00 3. Road Depth 16. Culvert Length ft 0.33 ft 200 **Roads Sub-Totals** 4. Aggregate Unit Cost 35.00 \$/yd3 17. Road Surface Cost 27,207 \$ 5. GeoTextile Length 0 ft 18. GeoTextile Cost 0 \$ 6. GeoTextile Unit Cost 0.00 \$/yd2 1,500 19. Silt Fence Cost \$ 7. Length of Silt Fence ft 500 10,000 20. Culvert Cost \$ 8. Unit Cost of Silt Fence \$/ft 3.00 21. Revegetation Cost 876 \$ **9**. Surveying? 0 22. Survey Cost \$ 10. Survey Rate acres/day 23. Clear and Grub Cost 0 \$ 11. Survey Unit Cost \$/day □ 12. Clearing and Grubbing? 24. Total Cost 39,583 \$ 13. Clear and Grub Cost \$/acre Record Number 1 of 1

Company Name <u>Stream Restoration Inc.</u> Project <u>O&M TAG</u>

Site Name Spaghetti Hole

AMD TREAT ENGINEERING COST



* Total Capital Cost minus Engineering and Land Access Capital Cost



Project O&M TAG

Site Name Spaghetti Hole

AMD TREAT

OTHER COST



AMOTREAT

| OTHER COST Oher Cost Name Spaghetti Hole Improvements | | | | AWDTREP | |
|---|--------------------------------|--|-----------------|-------------------------------------|---|
| | A. Description of Item | B. Unit Cost Per Item | C. Quantit | D. y Total Item Cost | E. Capital Cost Annual Cost |
| 1. | Clean sediment pond (CY) | 10.00 | 1000 | 10,000 | Capital Cost C Annual Cost |
| 2. | Excavate sediment pond (CY) | 10.00 | 800 | 8,000 | Capital Cost C Annual Cost |
| 3. | Remove SAP sediment (CY) | 10.00 | 1000 | 10,000 | Capital Cost C Annual Cost |
| 4. | Remove SAP compost (CY) | 10.00 | 2000 | 20,000 | Capital Cost C Annual Cost |
| 5. | Clean SAP Limestone (T) | 8.00 | 3500 | 28,000 | Capital Cost |
| 6. | Inlet flume with approach (EA) | 1.00 | 7000 | 7,000 | Capital Cost C Annual Cost |
| 7. | Misc pipe and materials (JOB) | 1.00 | 10000 | 10,000 | Capital Cost C Annual Cost |
| 8. | Mob/Demob (JOB) | 20,000.00 | 1 | 20,000 | Capital Cost C Annual Cost |
| 9. | E&S Controls (JOB) | 23,000.00 | 1 | 23,000 | Capital Cost C Annual Cost |
| 10. | | 0.00 | 0 | 0 | Capital Cost C Annual Cost |
| 11. | | 0.00 | 0 | 0 | Capital Cost |
| 12. | | 0.00 | 0 | 0 | Capital Cost C Annual Cost |
| 13. | | 0.00 | 0 | 0 | Capital Cost |
| 14. | | 0.00 | 0 | 0 | Capital Cost |
| 15. | | 0.00 | 0 | 0 | Capital Cost C Annual Cost |
| - | Record Number 1 of 1 | Curent Capital Cost 136 Current Annual Cost | ,000 \$ 0 \$ | Total Capital Co Total Annual Co | · |